

# High-Order Boundary Integral Methods for Slender Bodies

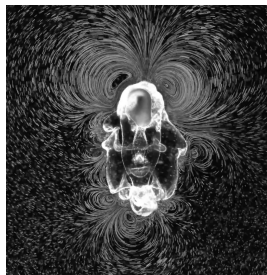
Dhairya Malhotra, Alex Barnett



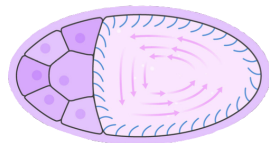
March 1, 2023

# Motivations

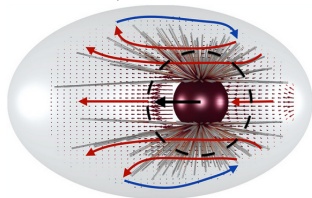
Stokes simulations with fibers are key to modeling complex fluids (suspensions, rheology, industrial, biomedical, cellular biophysics).



Starfish larvae  
(Gilpin et al. 2016)



Drosophila oocyte  
(Stein et al. 2021)



Mitotic spindle (Nazockdast et al. 2015)

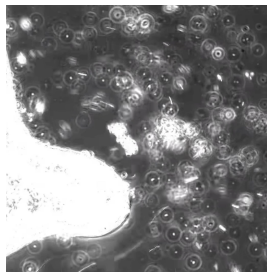


# Motivations

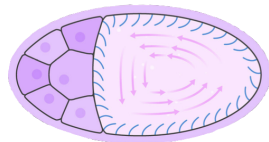
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## Slender Body Theory (SBT):

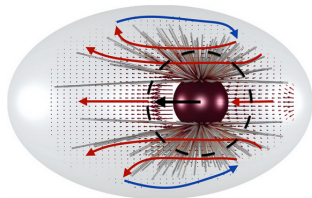
- Asymptotic expansion in radius ( $\varepsilon$ ) as  $\varepsilon \rightarrow 0$  (Keller-Rubinow '76).
- Doublet correction to make velocity theta-independent (Johnson '80).



Starfish larvae  
(Gilpin et al. 2016)



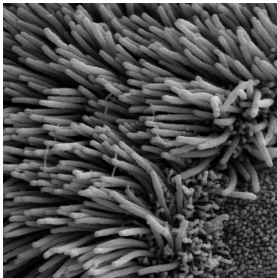
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**Error estimates:** Rigorous analysis difficult (few very recent studies)

- classical asymptotics claims:  $\varepsilon^2 \log(\varepsilon)$
- rigorous analysis:  $\varepsilon \log^{3/2}(\varepsilon)$  (Mori-Ohm-Spirn '19)
- numerical tests:  $\varepsilon^{1.7}$  (Mitchell et al. '21 -- verify close-touching breakdown)  
close-to-touching with gap of  $10\varepsilon$ , only 2.5-digits in the infy-norm.  
 $\varepsilon=1e-2$  only 1-2 digits achievable by SBT.

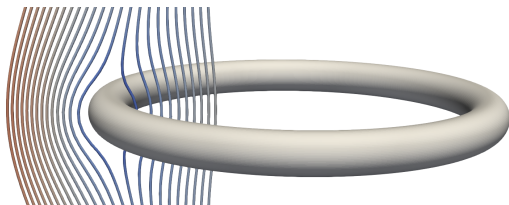


Source: <http://remf.dartmouth.edu/imagesindex.html>

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$\varepsilon$	$\mathbf{u}_{exact}$	Rel-Error
1e-1	6.1492138359856e-2	0.5e-2
1e-2	9.0984522324584e-2	0.1e-3
1e-3	1.2015655889904e-1	0.2e-5
1e-4	1.4931932907587e-1	0.2e-7
1e-5	1.7848191313097e-1	0.3e-9



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**Limitations of SBT:**

- no convergence analysis for fibers of given nonzero radius.
- uncontrolled errors when fibers close  $O(\varepsilon)$ .

Efficient convergent BIE method needed, allowing adaptivity for close interactions.

# Goals

Solve the slender body BVP

- in a convergent way.
- adaptively when fibers become close.
- efficiently with effort independent of radius.

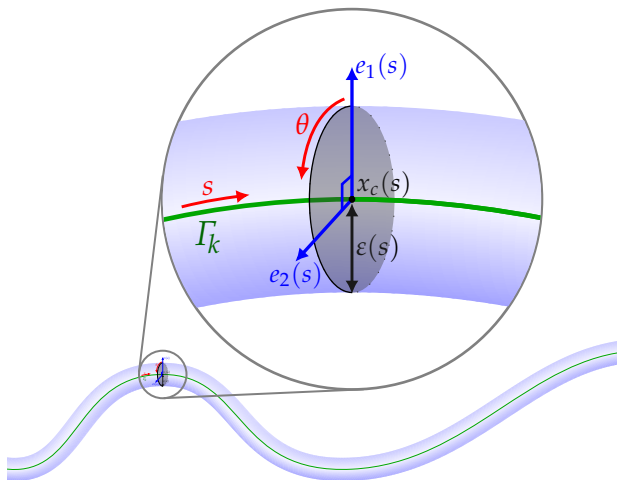
Validate current SBT simulations.

Focus on rigid fibers in this talk -- flexible fibers for future.

*Related work:* Mitchell et al, '21 (mixed-BVP corresponding to flexible fiber loop)

## Geometry description:

- parameterization  $s$  along fiber length
- coordinates  $x_c(s)$  of centerline curve
- circular cross-section with radius  $\varepsilon(s)$
- orientation vector  $e_1(s)$



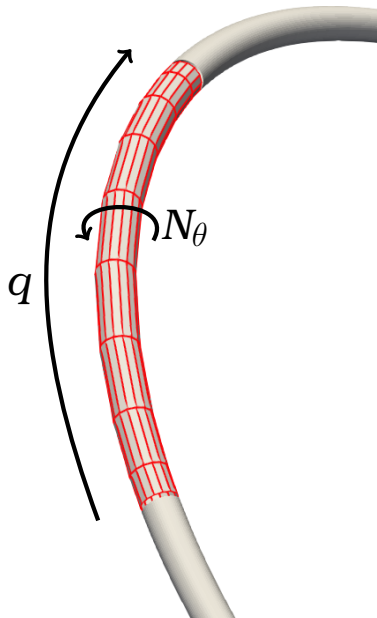
# Discretization

## Geometry description:

- parameterization  $s$  along fiber length
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- orientation vector  $e_1(s)$

## Discretization:

- piecewise Chebyshev (order  $q$ ) discretization in  $s$  for  $x_c(s)$ ,  $\varepsilon(s)$ ,  $e_1(s)$
- Collocation nodes: tensor product of Chebyshev and Fourier discretization in angle with order  $N_\theta$ .



# Boundary Quadratures

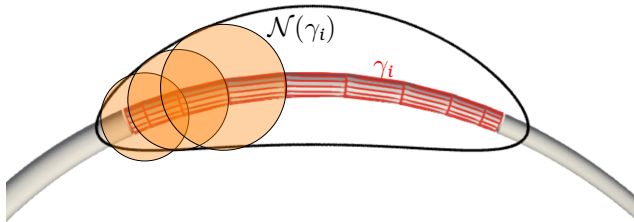
$$\begin{aligned} u(\mathbf{x}) &= \int_{\Gamma} \mathcal{K}(\mathbf{x} - \mathbf{y}) \sigma(\mathbf{y}) \, d\mathbf{a}(\mathbf{y}) = \sum_{k=1}^{N_{\text{panel}}} \int_{\gamma_k} \mathcal{K}(\mathbf{x} - \mathbf{y}) \sigma(\mathbf{y}) \, d\mathbf{a}(\mathbf{y}) \\ &= \underbrace{\sum_{\mathbf{x} \notin \mathcal{N}(\gamma_k)} \int_{\gamma_k} \mathcal{K}(\mathbf{x} - \mathbf{y}) \sigma(\mathbf{y}) \, d\mathbf{a}(\mathbf{y})}_{\text{far-field}} + \underbrace{\sum_{\mathbf{x} \in \mathcal{N}(\gamma_k)} \int_{\gamma_k} \mathcal{K}(\mathbf{x} - \mathbf{y}) \sigma(\mathbf{y}) \, d\mathbf{a}(\mathbf{y})}_{\text{near interactions}} \end{aligned}$$



$$\begin{aligned} u(x) &= \int_{\Gamma} \mathcal{K}(x-y) \sigma(y) da(y) = \sum_{k=1}^{N_{panel}} \int_{\gamma_k} \mathcal{K}(x-y) \sigma(y) da(y) \\ &= \underbrace{\sum_{x \notin \mathcal{N}(\gamma_k)} \int_{\gamma_k} \mathcal{K}(x-y) \sigma(y) da(y)}_{\text{far-field}} + \underbrace{\sum_{x \in \mathcal{N}(\gamma_k)} \int_{\gamma_k} \mathcal{K}(x-y) \sigma(y) da(y)}_{\text{near interactions}} \end{aligned}$$

## Far field approximation:

- Gauss-Legendre quadrature in  $s$ .
- periodic trapezoidal rule in  $\theta$ .
- determine  $\mathcal{N}(\gamma_k)$  using standard error estimates



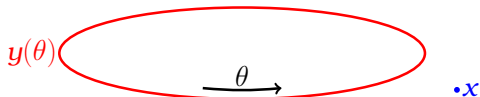
# Boundary Quadratures

**Near interactions:** for  $x \in \mathcal{N}(\gamma_k)$

$$\int_{\gamma_k} \mathcal{K}(x - y) \sigma(y) da(y) = \int_s \int_{\theta} \mathcal{K}(x - y(s, \theta)) \sigma(s, \theta) J(s, \theta) d\theta ds$$

**Inner integral in  $\theta$ :**

- potential from a ring source  
-- modal Green's function.
- can be nearly singular as  $x \rightarrow \gamma_k$ .



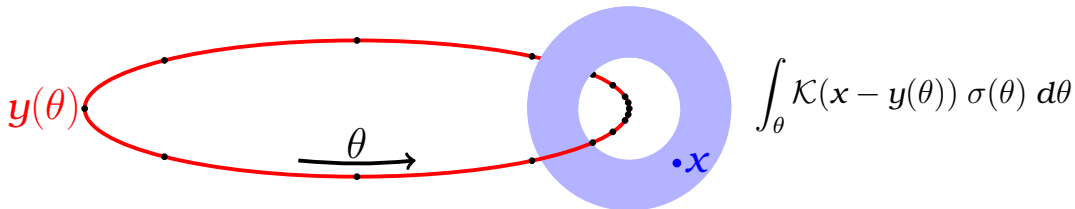
**Outer integral in  $s$ :**



# Fast Modal Green's Function Evaluation

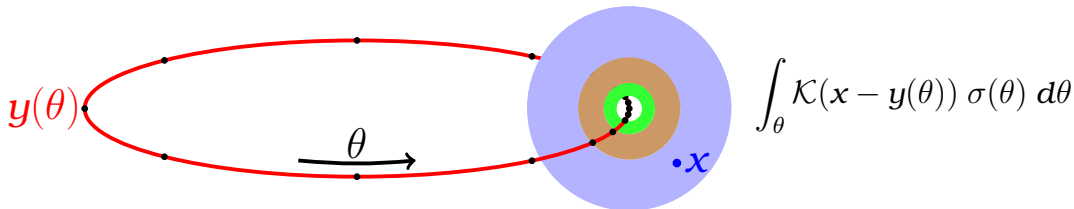
$y(\theta)$   $\xrightarrow{\theta}$   $\bullet x$   $\int_{\theta} \mathcal{K}(x - y(\theta)) \sigma(\theta) d\theta$

- Analytic representation in special functions - Young, Hao, Martinsson JCP-2012
  - modal Green's functions -- method of choice for axisymmetric problems.



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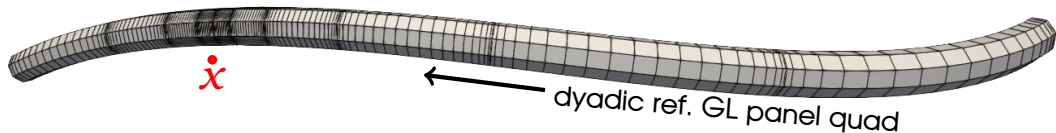


- Analytic representation in special functions - Young, Hao, Martinsson JCP-2012
  - modal Green's functions – method of choice for axisymmetric problems.
- Build special quadrature rules!
  - e.g. generalized Gaussian quadratures: Bremer, Gimbutas and Rokhlin - SISC 2010.
  - Different rule for each nested annular region (up to  $10^{-6}$  from source).
    - ~ 48 quadrature nodes for  $n_0 = 8$  and 10-digits accuracy.
    - ~ 26M modal Green's function evaluations/sec/core (Skylake 2.4GHz)

# Quadratures for Outer Integral

**Near Interactions:**  $x$  is off-surface or adjacent panel

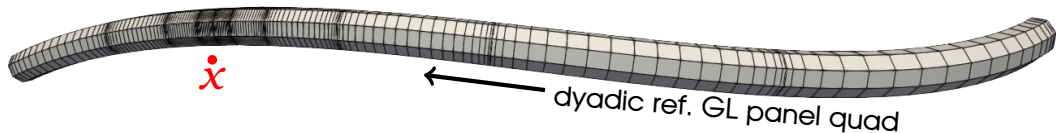
- panel (Gauss-Legendre) quadrature with dyadic refinement.



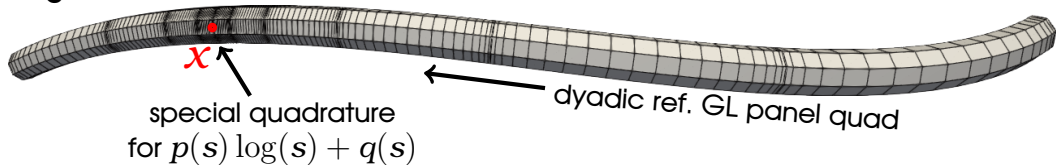
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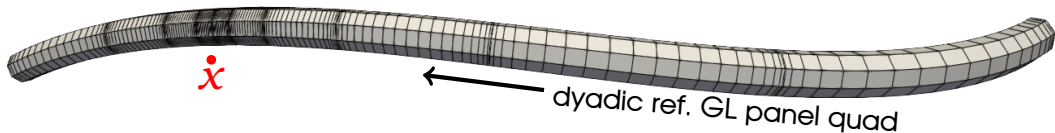
**Singular Interactions:**  $x$  is on-surface



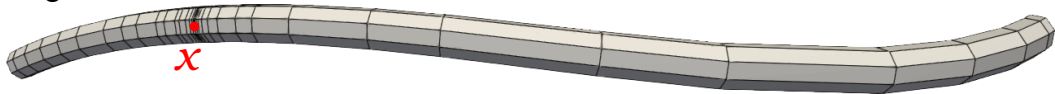
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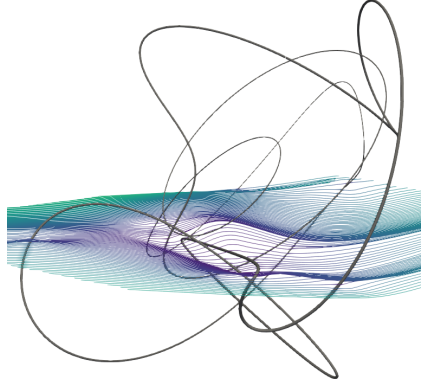
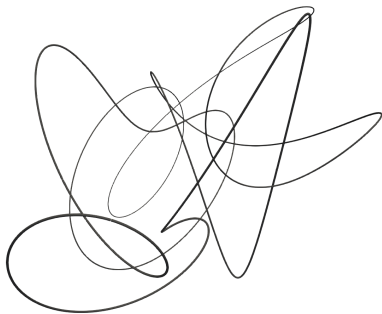


*Instead build special quadrature rules!*

- replace composite panel quadratures with a single quadrature.
- Separate rules for different aspect ratios ( $1 - 10^4$  in powers of 2)



# Numerical Results - Stokes BVP



## Exterior Stokes

**Dirichlet BVP:**

$$\Delta \mathbf{u} - \nabla p = 0,$$

$$\nabla \cdot \mathbf{u} = 0,$$

$$\mathbf{u}|_{\Gamma} = \mathbf{u}_0,$$

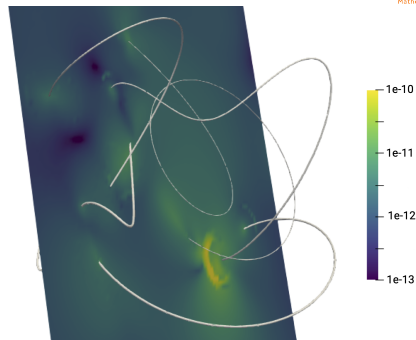
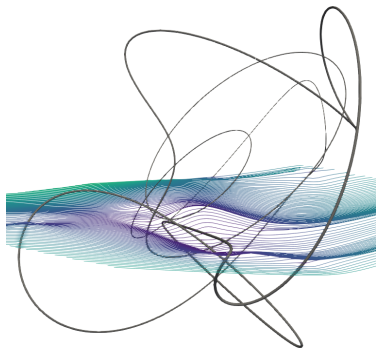
$$u(\mathbf{x}) \rightarrow 0 \text{ as } |\mathbf{x}| \rightarrow \infty,$$

wire radius =  $1.5e-3$  to  $4e-3$

wire length = 16

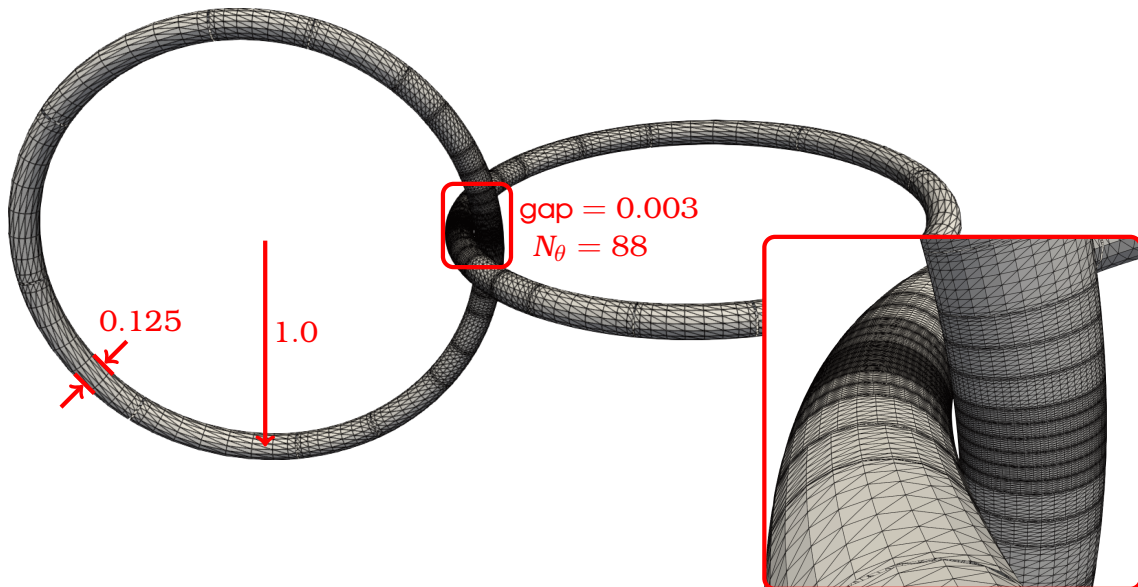
**BIE formulation:**  $(\mathcal{I}/2 + \mathcal{D} + \mathcal{S} / (2\varepsilon \log \varepsilon^{-1}))[\boldsymbol{\sigma}] = \mathbf{u}_0$

# Numerical Results - Stokes BVP

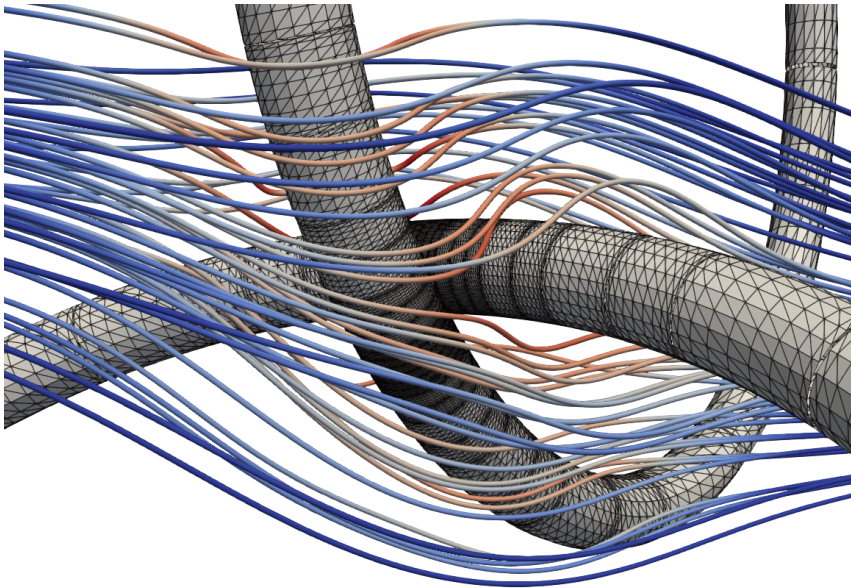


$N$	$N_{panel}$	$N_{\theta}$	$\epsilon_{GMRES}$	$N_{iter}$	$\ e\ _{\infty}$	1-core			40-cores	
						$T_{setup}$	$(N/T_{setup})$	$T_{solve}$	$T_{setup}$	$T_{solve}$
1.5e4	122	4	1e-03	10	1.9e-02	0.33	(4.4e4)	0.7	0.024	0.05
9.1e4	252	12	1e-05	21	1.7e-04	3.31	(2.7e4)	61.2	0.197	5.25
9.4e4	262	12	1e-07	33	4.1e-06	4.43	(2.1e4)	104.3	0.224	7.69
2.0e5	272	24	1e-09	43	1.4e-08	17.70	(1.1e4)	586.0	0.796	22.94
2.3e5	276	28	1e-11	54	4.1e-09	27.67	(8.4e3)	1034.2	1.229	38.85

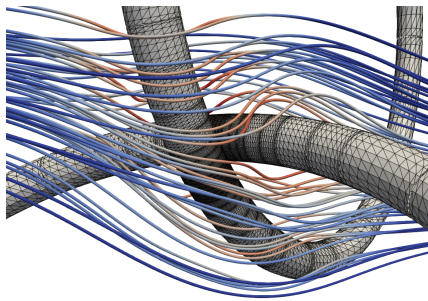
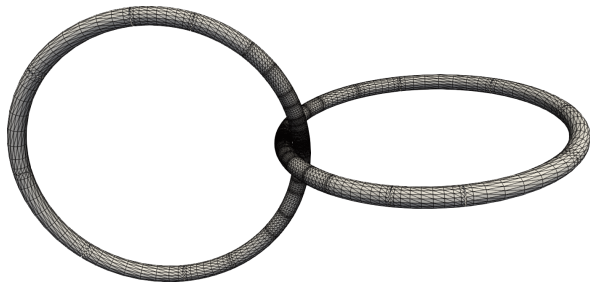
# Numerical Results - close-to-touching



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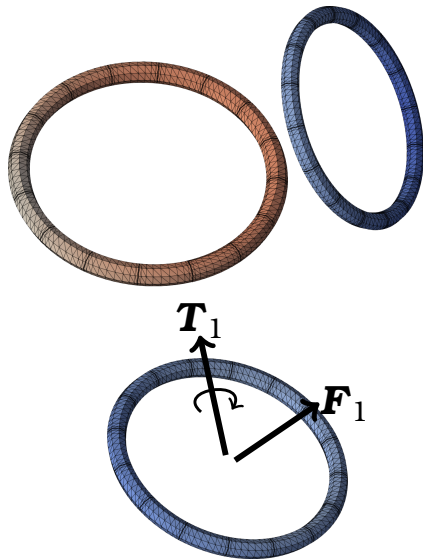
$N$	$\epsilon_{GMRES}$	$N_{iter}$	$\ e\ _{\infty}$	1-core		40-cores		
				$T_{setup}$	$(N/T_{setup})$	$T_{solve}$	$T_{setup}$	$T_{solve}$
6.5e4	1e-02	4	2.1e-02	8.1	(8.0e+3)	6.5	1.28	1.4
6.5e4	1e-05	24	2.4e-03	16.8	(3.8e+3)	42.9	2.50	7.7
6.5e4	1e-07	43	2.8e-06	23.5	(2.7e+3)	81.6	3.31	12.8
6.5e4	1e-10	59	5.4e-08	35.6	(1.8e+3)	122.9	4.06	19.2
6.5e4	1e-13	72	1.3e-10	49.9	(1.3e+3)	162.6	5.27	23.2

# Mobility problem

- $n$  rigid bodies  $\Omega = \sum_{i=1}^n \Omega_i$   
with velocities  $\mathbf{V}(\mathbf{x}) = \mathbf{v}_i + \boldsymbol{\omega}_i \times (\mathbf{x} - \mathbf{x}_i^c)$ ,  
and given forces  $\mathbf{F}_i$ , torques  $\mathbf{T}_i$  about  $\mathbf{x}_i^c$ .

- Stokesian fluid in  $\mathbb{R}^3 \setminus \Omega$   
$$\Delta \mathbf{u} - \nabla p = 0, \quad \nabla \cdot \mathbf{u} = 0,$$
  
$$\mathbf{u} \rightarrow 0 \text{ as } \mathbf{x} \rightarrow \infty.$$

- Boundary conditions on  $\partial\Omega$ ,  
$$\mathbf{u} = \mathbf{V} + \mathbf{u}_s.$$



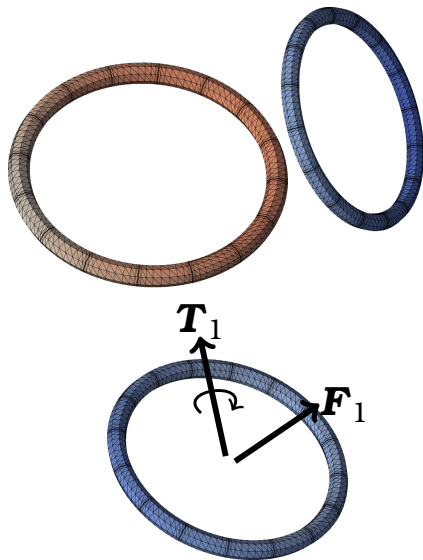
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unknown:  $\mathbf{V}(\mathbf{u}_i, \boldsymbol{\omega}_i)$



# Mobility problem - double-layer formulation

Represent fluid velocity:  $\mathbf{u} = \mathcal{S}[\boldsymbol{\nu}(\mathbf{F}_i, \mathbf{T}_i)] + \mathcal{D}[\boldsymbol{\sigma}]$

and rigid body velocity:  $\mathbf{V} = - \sum_{i=1}^{6n} \mathbf{v}_i \mathbf{v}_i^T \boldsymbol{\sigma}$

Applying boundary conditions ( $\mathbf{u} = \mathbf{V} + \mathbf{u}_s$  on  $\partial\Omega$ ),

$$(\mathcal{I}/2 + \mathcal{D})[\boldsymbol{\sigma}] + \sum_{i=1}^{6n} \mathbf{v}_i \mathbf{v}_i^T \boldsymbol{\sigma} = \mathbf{u}_s - \mathcal{S}[\boldsymbol{\nu}]$$

*(Pozrikidis - Boundary Integral and Singularity Methods for Linearized Viscous Flow)*



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Second kind integral equation, should be well-conditioned.

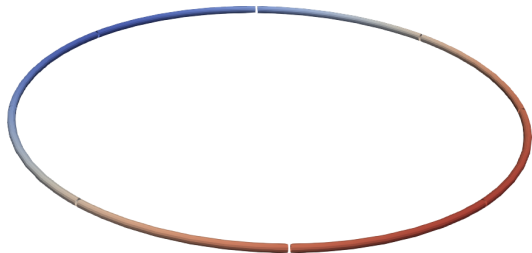
What can possibly go wrong?

# Conditioning of layer-potential operators

$$\kappa(\mathcal{S}) \quad \sim 2.6e6$$

$$\kappa(\mathcal{I}/2 + \mathcal{D}) \quad \sim 4.3e6$$

$$\kappa(\mathcal{I}/2 + \mathcal{D} + 16\mathcal{S}) \quad \sim 80$$



- For infinite cylinder (Laplace case):  $\kappa(\mathcal{I}/2 + \mathcal{D}) \sim \varepsilon^{-2} \log^{-1} \varepsilon^{-1}$
- Combined field operator well-conditioned:  $\mathcal{I}/2 + \mathcal{D} + \mathcal{S} / (2\varepsilon \log \varepsilon^{-1})$

# Mobility problem - combined field formulation

Represent fluid velocity:  $\mathbf{u} = \mathcal{S}[\boldsymbol{\nu}(\mathbf{F}_i, \mathbf{T}_i)] + \mathcal{K}[\boldsymbol{\sigma}]$

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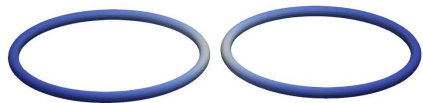
Second kind integral equation and well-conditioned!

# Numerical Results - Sedimentation Flow

**Time-stepping:** 5-th order adaptive SDC

**8-digits accuracy** in quadratures, GMRES solve,  
and time-stepping.

**40 CPU cores**

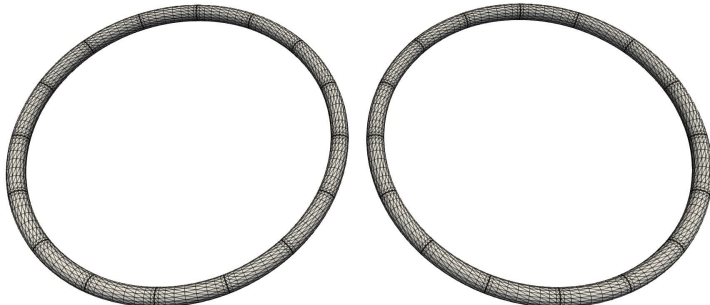
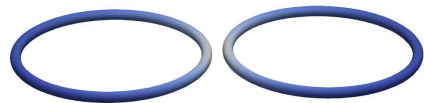


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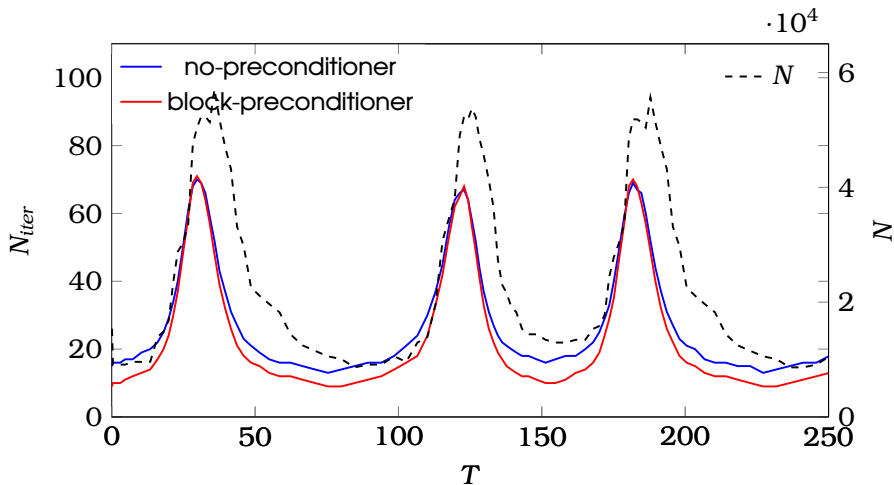
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# Numerical Results - Sedimentation Flow



**Close-to-touching:** smaller time-steps, more unknowns ( $N$ ),  
high GMRES iteration count (block preconditioner doesn't help).

$\sim 125\times$  more expensive!

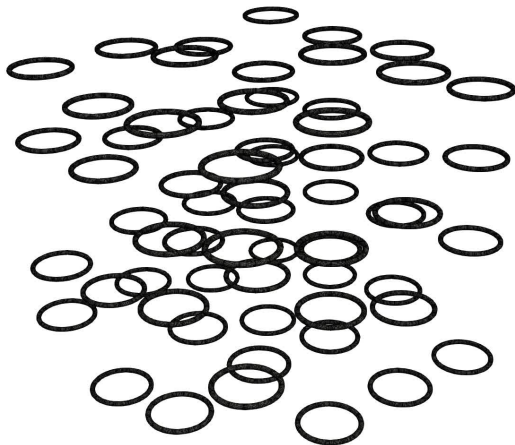


**5-th order adaptive SDC**

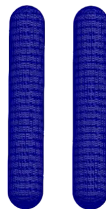
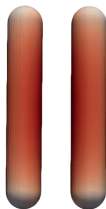
**8-digits accuracy** in  
quadratures, GMRES solve,  
and time-stepping.

**0.5 million unknowns**  
64 rings.

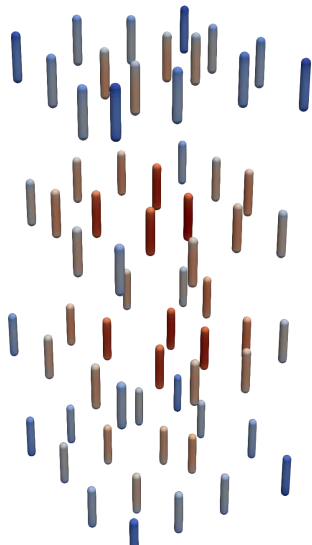
**160 CPU cores**



# Numerical Results - Sedimentation Flow



# Numerical Results - Sedimentation Flow



# Conclusions

- Convergent boundary integral formulation for slender bodies.
  - unlike SBT, boundary conditions are actually enforced to high accuracy.
- Special quadratures - efficient for aspect ratios as large as  $10^5$ .
  - quadrature setup rates up to 20,000 unknowns/s/core (comparable to FMM speeds).
- Stokes mobility problem - combined field BIE formulation.
  - well-conditioned formulation for slender-body geometries.
  - high-order time stepping (SDC), block-diagonal preconditioner.

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## Limitations and ongoing work:

- Open problems: collisions, better preconditioners.
- Flexible fibers -- applications in biological fluids.